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APPLICATION
FOR
UNITED STATES LETTERS PATENT

Be it known that we, Reinhardt L. Willig, residing at 7 Sunset Road, Maynard,
MA 01754 and being a citizen of the United States; William P. Kelleher, residing at 3
10 Betsy Ross Circle, Acton, MA 01720 and being a citizen of the United States; and
Stephen P. Smith, residing at 77 Sherwood Road, Medford, MA 02155 and being a
citizen of Canada, have invented a certain new and useful

PHOTONIC CRYSTAL INTERFEROMETRIC FIBER OPTICAL GYROSCOPE
SYSTEM

15 of which the following is a specification:

Applicant: Willig *et al.*
For: PHOTONIC CRYSTAL INTERFEROMETRIC FIBER OPTICAL
GYROSCOPE SYSTEM

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RELATED APPLICATIONS

This application claims priority of United States Provisional Application No. 60/426,264 filed November 13, 2002, incorporated by reference herein.

GOVERNMENT RIGHTS

10 This invention was made with U.S. Government support under Contract No. N00030-01-C-0022 awarded by the U.S. Navy. The Government may have certain rights in the subject invention.

FIELD OF THE INVENTION

15 This invention relates generally to gyroscope systems and more particularly to an improved photonic crystal interferometric fiber optical gyroscope (IFOG) system.

BACKGROUND OF THE INVENTION

Gyroscopes may be used to measure an angular change in direction. Conventional IFOGs employ, *inter alia*, a sensing coil to measure the rate of rotation of the gyroscope. The sensing coil of the IFOG typically includes an optical fiber wound on a mandrel or into a freestanding coil. Light is introduced to the rotating sensing coil and an optical splitter splits the light into two counter-propagating beams. One beam is propagated in the same direction as the rotating coil and the other beam is propagated in the direction opposite the direction of the rotating coil. Because light propagating in the same

direction of rotation as the sensing coil travels a longer distance than the light propagating in the opposite direction of the sensing coil, a phase shift results when the counter propagating beams return to the optical splitter. A detector is used to measure the power of the counter-propagating beams of light which represents the phase shift between the
5 two counter-propagating beams. The relative phase shift of the counter-propagating beams is indicative of the rate of rotation of the sensing coil about its axis. The fundamental measure of the precision of the rate of rotation of an IFOG is known as angle random walk (ARW), measured in degrees per square root hours (degree/ \sqrt{hr}). The ability to measure power of the counter-propagating beams represents the sensitivity of
10 the IFOG.

For a sensing coil with a fixed volume and low-loss optical fiber, the precision of an IFOG, as indicated by the ARW, is proportional to the square of the fiber diameter. This is because the ARW is inversely proportional to the length of the fiber in the sensing coil and the length of the fiber is inversely proportional to the square of the fiber
15 diameter. Hence, the ARW of the sensing coil can be improved by using fiber with a reduced diameter and/or increased length. The ARW can also be improved by increasing the spectral width of the light source of the IFOG because the ARW of an IFOG is inversely proportional to the square root of the spectral width. Hence, increasing the spectral width of the light source reduces the ARW. However, the light source of a
20 conventional IFOG is limited by the bandwidth of the fiber. A conventional optical fiber could be designed to have a bandwidth of several hundred nanometers. However, increasing the bandwidth increases the bend loss in the fiber. In practice, when a conventional fiber is employed in an IFOG, the fiber is typically designed to have a

bandwidth of less than 100 nm to minimize bend loss of the fiber.

One technique to improve sensitivity of an IFOG is to increase the number of turns of the optical fiber in the sensing coil thereby increasing the length of the optical fiber which increases the phase difference between the counter propagating beams of light in the sensing coil. Increasing the phase difference between the counter-propagating beams changes the power such that the ability of the detector to measure the power improves, thereby improving the sensitivity of the IFOG. However, increasing the number of turns of optical fiber in the sensing coil increases the size of the sensing coil, which increases package diameter of the IFOG. A typical prior IFOG manufactured with conventional optic fiber would have a package diameter of about 3 inches.

Typical conventional optical fibers employed in the sensing coils of prior IFOGs include a solid center core surrounded by a solid clad. The solid core is used to transmit light while the clad reflects the light within the core. Typically, the optical fiber is designed such that the index of refraction of the core (n_1) is greater than the index of refraction of the clad (n_2) thereby totally reflecting the light at the core-cladding interface. However, the conventional optical fibers utilized in the sensing coils of prior IFOGs have significant loss of light (bend loss) due to bending associated with winding the fiber into a sensing coil, which decreases both the accuracy and precision of the IFOG.

The majority of prior IFOG sensing coils are made with glass fibers that are made with silica (SiO_2). For silica based fibers, the index difference needed to confine the light within the core is accomplished by either adding a dopant to the core of the fiber (up-doping) or adding a dopant to the cladding of the fiber (down-doping). For example, germanium or phosphorus may be added to the core of the fiber (up-doped) or fluorine or

boron may be added to the cladding (down-doped).

One prior attempt to overcome the large bend loss associates with conventional optical fibers utilized in sensing coils of prior IFOGs is to increase the index difference between the core and the clad, e.g., the index difference between n_1 and n_2 . Increasing the index difference decreases the bend loss because it increases the degree to which light is confined inside the core of fiber.

The most common fiber used in conventional IFOG sensing coils is a silica based fiber where the core is up-doped with germanium. The bend loss in the sensing coils made with these fibers can be decreased by increasing the amount of germanium in the core. However, there are two limitations to up-doping the core. First, the amount of index change that can be obtained by doping silica with germanium is less than ten percent. Second, because the material properties of doped silica are different from those of undoped silica, the manufacturing process used to make the fiber introduces more and more defects as the amount of germanium is increased. These defects increase the amount of light absorbed by the fiber per unit length.

Another drawback to conventional IFOG sensing coils made with germanium doped optical fiber is that this fiber can be damaged by gamma radiation. Most dopants, like germanium, increase the degree to which gamma radiation causes ionization in the fiber. This ionization increases the optical loss of the fiber and hence decreases the precision of the IFOG.

One prior art attempt to overcome the gamma radiation sensitivity and the length loss problems associated with germanium doped optical fibers is to dope the clad with fluorine to decrease the index of refraction of the clad n_2 (e.g., increase the difference of

the index of refraction between n_1 and n_2 by decreasing n_2). Fluorine absorbs less light and less gamma radiation than germanium. However, there is a limit to the difference between the index of refraction between the core (n_1) and the clad (n_2), hence, fluorine doped fibers have limited ability to reduce bend loss.

5 Conventional optical fibers utilized in the sensing coil of prior IFOGs are also thermal and ionization radiation sensitive.

SUMMARY OF THE INVENTION

It is therefore an object of this invention to provide a photonic crystal
10 interferometric fiber optical gyroscope system.

It is a further object of this invention to provide such a system which is more accurate.

It is a further object of this invention to provide such a system which is more sensitive.

15 It is a further object of this invention to provide such a system which reduces the ARW.

It is a further object of this invention to provide such a system which increases the usable spectral width of the light source.

20 It is a further object of this invention to provide such a system which reduces bend loss.

It is a further object of this invention to provide such a system which reduces length loss.

It is a further object of this invention to provide such a system which reduces

sensitivity to ionization radiation.

It is a further object of this invention to provide such a system which reduces thermal sensitivity.

5 It is a further object of this invention to provide such a system which reduces thermal gradient sensitivity.

It is a further object of this invention to provide such a system which eliminates the need to use dopants in the optical fiber of the sensing coil to decrease bend loss, decrease length loss, or improve radiation sensitivity.

It is a further object of this invention to provide such a system which reduces the 10 package size of the IFOG.

This invention results from the realization that a truly effective photonic crystal interferometric optical gyroscope system is achieved by: 1) an improved light source which provides light with an increased spectral width; 2) a unique photonic sensing coil which includes photonic optical fibers with a gas-solid structure that confines light by 15 total internal reflection (TIR) or band gap optical fibers that confine light by employing an optical band gap; and/or 3) a beam controlling device which splits the light into counter-propagating beams in the photonic crystal sensing coil and directs the return of the counter-propagating beams whose power represents the phase shift between the counter-propagating beams which is indicative of the rate of rotation of coil.

20 This invention features a photonic crystal interferometric optical gyroscope system including a light source for providing a primary beam of light, a photonic crystal sensing coil having a rotational axis, and a beam controlling device configured to split the primary beam into first and second counter-propagating beams in the photonic crystal

sensing coil and configured to direct return of the counter-propagating beams wherein the power of the returning counter-propagating beams represents the phase shift between the counter-propagating beams and is indicative of the rate of rotation of the coil about the rotational axis.

5 In a preferred embodiment, the photonic crystal sensing coil may be formed by winding a photonic crystal fiber having a gas-solid structure that confines the light by total internal reflection or may be formed by winding a band gap fiber which confines the light by employing an optical band gap. The photonic crystal fiber may be configured to maintain the polarization of the first and second counter-propagating beams. The
10 photonic crystal fiber may be configured to propagate only one state of polarization of the first and second counter-propagating beams. The photonic crystal fiber may be configured to propagate a single mode of light. The band gap fiber may be configured to maintain the polarization of the light. The band gap fiber may be configured to propagate only one state of polarization of the light. The band gap fiber may be configured to
15 propagate a single mode of light. The photonic crystal sensing coil may include 15,000 turns of the photonic crystal fiber or may include 35,000 turns of the photonic crystal fiber. The photonic crystal sensing coil may include 15,000 turns of the band gap fiber or may include 35,000 turns of the band gap fiber. The photonic crystal fiber may include a solid core region surrounded by solid clad having a plurality of hollow channels
20 configured to provide an index of refraction difference between the solid core region and the clad that confines light in the core by totally reflecting light on the clad and propagates a single mode of light. The photonic crystal fiber may include a jacket surrounding the clad. The photonic crystal fiber may have an outer diameter in the range

of about 20 to 250 microns. The photonic crystal fiber may have an outer diameter in the range of about 70 microns. The photonic crystal fiber may have an outer diameter of about 40 microns. The solid core and the clad may be made of silica, and/or plastic, and/or a dielectric material. The band gap fiber may include a hollow core region

5 surrounded by a solid clad including a plurality of hollow channels configured to define a band gap which confines the majority of light in the hollow core region and propagates a single mode of light. The band gap fiber may include a jacket surrounding the clad. The band gap fiber may have an outer diameter in the range of about 20 to 250 microns. The band gap fiber may have an outer diameter of about 70 microns. The band gap fiber may

10 have an outer diameter of about 40 microns. The clad may be made of silica, and/or plastic, and/or a dielectric material. The band gap fiber may include a hollow core region surrounded by solid clad having a plurality of alternating layers of solid dielectric material, the alternating layers of dielectric material configured to create a band gap effect that confines the majority of light in the hollow core region and propagates a single mode

15 of light. The band gap fiber may further include a jacket surrounding the clad. The band gap fiber may have an outer diameter in the range of about 20 to 250 microns. The band gap fiber may have an outer diameter of about 70 microns. The band gap fiber may have an outer diameter of about 40 microns. The alternating layers of solid electric material may include silica and/or plastic. The alternating layers of solid electric material may

20 include a material chosen from the group consisting of silica, doped silica, fluoride glasses, chalcogenide glasses and thermoplastic polymers. The photonic crystal fiber may include an asymmetric solid core region surrounded by a solid clad having a plurality of asymmetrically spaced hollow channels about the solid core region to provide an index of

refraction difference between the core region and the clad that confines the light by totally reflecting light on the hollow channels of the clad and maintains the polarization of the light. The band gap fiber may include an asymmetric hollow region surrounded by a solid clad having a plurality of asymmetrically spaced hollow channels configured to define a

5 band gap effect that confines the majority of light in the hollow core and maintains the polarization of the light. The band gap fiber may include an asymmetric hollow core region surrounded by a plurality of alternating asymmetric layers of solid dielectric material configured to define a band gap effect that confines the majority of light in the core region and maintains the polarization of the light. The photonic crystal fiber may

10 include an asymmetric solid core region surrounded by a solid clad having a plurality of asymmetrically spaced hollow channels about the solid core region configured to provide an index of refraction difference between the core region and the clad that confines light by totally reflecting light on the hollow channels of the clad and propagates the one state of polarized light. The band gap fiber may include an asymmetric hollow region

15 surrounded by a solid clad having a plurality of asymmetrically spaced hollow channels configured to define a band gap that confines the majority of light in the hollow core and propagates the one state of polarized light. The band gap fiber may include an asymmetric hollow core region surrounded by clad including a plurality of alternating asymmetric layers of solid dielectric material configured to define a band gap that

20 confines the majority of light in the core region and propagates one state of polarized light. The photonic crystal sensing coil may have an outer diameter, an inner diameter, and a height, the outer diameter may be in the range of about 0.5 inches to 9 inches, the inner diameter may be in the range of about 0.5 to 8 inches, and the height may be in the

range of about 0.25 to 4 inches. The photonic crystal sensing coil may have an outer diameter of about 2.0 inches, an inner diameter of about 1.5 inches, and a height of about 1.0 inch. The photonic crystal sensing coil may have an outer diameter of about 0.75 inches, an inner diameter of about 0.5 inches, and a height of about 0.75 inches. The

5 photonic crystal interferometric optical gyroscope system may include an optical wave guide configured to interconnect the light source and the beam controlling device and/or the beam controlling device and photonic crystal sensing coil. The optical wave guide may be chosen from the group consisting of a solid structure wave guide that confines the light by total internal reflection, a photonic crystal wave guide having a gas-solid

10 structure that confines the light by total internal reflection, and a band gap wave guide that confines the light by employing an optical band gap. The solid structure wave guide may be configured as an optical fiber. The photonic crystal wave guide may be configured as photonic crystal fiber. The band gap wave guide may be configured as a band gap optical fiber. The optical fiber, the photonic crystal fiber, and the band gap fiber may be configured to maintain the polarization of the light. The optical fiber, the photonic crystal fiber, and the band gap fiber may be configured to propagate only one state of polarization of the light. The optical fiber, the photonic crystal fiber, and the band gap fiber may be configured to propagate a single mode of light. The beam

15 controlling device may include first and second optical splitters and a least one phase modulator. The first optical splitter may be a reciprocal splitter. The first optical splitter may be a non-reciprocal splitter. The first optical splitter may be configured to direct light from the light source to a coil splitter and direct the return of the first and second counter-propagating beams from the sensing coil to a light detector. The first optical

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splitter may be configured as a broad-band splitter to transmit light with a spectral width up to about 1500 nm. The second optical splitter may be a reciprocal splitter. The second optical splitter may be configured to divide the light from the light source into two equal
the first and second counter-propagating beams. The at least one phase modulator may be
5 configured to add a time dependent phase shift to the first and second counter-
propagating beams to produce a non reciprocating phase shift between the first and
second counter-propagating beams such that the first and second counter-propagating
beams constructively interfere to modify the power thereby improving the precision of the
system. The photonic crystal interferometric optical gyroscope system may further
10 include a photo detector configured to convert the power to an electrical signal. The
photo detector may be chosen from the group consisting of: a PIN photo detector, an
avalanche photo detector, a photo multiplier tube, a bolometer, a photo resistive detector,
and a photo conductive detector. The light source may provide the primary beam of light
having a wavelength in the range of about 100 nm to 15,000 nm. The light source may
15 provide the primary beam of light having a wavelength of about 1200 nm. The light
source may be chosen from the group consisting of an amplified spontaneous emission
light source, a stimulated emission light source, a thermally excited light source, a
fluorescent light source, an electro-luminescence light source, a chemical luminescence
light source, and a phosphorescence light source. The amplified spontaneous emission
20 light source may include a semiconductor material. The amplified spontaneous emission
light source may include a gas filled fiber and/or a rare earth doped fiber. The gas may be
chosen from the group consisting of argon, helium neon, carbon dioxide and carbon
monoxide. The amplified spontaneous light source may include a liquid filled fiber. The

liquid may include an organic dopant. The stimulated emission light source may include a laser. The stimulated emission light source may be chosen from the group consisting of a helium-neon doped fiber with a cavity, an argon doped fiber with a cavity, a carbon dioxide doped fiber with a cavity, and a semiconductor material with a cavity. The
5 thermally excited light source may include an incandescent light bulb. The fluorescent light source may include a fluorescent light bulb. The light source may be a broad-band light source which emits light with a spectral width of up to 1500 nm. The light source may be a broad-band light source which emits light with a spectral width of about 1200 nm. The photonic crystal sensing coil may have an ARW of about 0.001 degree/ $\sqrt{\text{hr}}$.
10 The photonic crystal sensing coil may have an ARW of about 0.00005 degree/ $\sqrt{\text{hr}}$.

This invention further features a photonic crystal interferometric optical gyroscope system including a broad-band light source for providing a primary beam of light with increased spectral width, a photonic crystal sensing coil having a rotational axis, and a beam controlling device configured to split the primary beam into first and second
15 counter-propagating beams in the photonic crystal sensing coil and configured to direct return of the counter-propagating beams; wherein the power of the returning counter-propagating beams represents the phase shift between the counter-propagating beams and is indicative of the rate of rotation of the coil about the rotational axis.

In one embodiment, the light source may be a tungsten-halogen light source. The
20 primary beam of light may have a spectral width of up to about 1500 nm. The photonic crystal sensing coil may be formed by winding a photonic crystal fiber having a gas-solid structure that confines the light by total internal reflection. The photonic crystal sensing coil may be formed by winding a band gap fiber which confines the light by employing an

optical band gap.

BRIEF DESCRIPTION OF THE DRAWINGS

Other objects, features and advantages will occur to those skilled in the art from
5 the following description of a preferred embodiment and the accompanying drawings, in
which:

Fig. 1 is a schematic block diagram showing several of the primary components of
a photonic crystal interferometric fiber optical gyroscope system in accordance with this
invention;

10 Figs. 2A-2F are schematic two-dimensional views showing typical photonic
crystal fibers and band-gap fibers employed in the photonic sensing coil and to
interconnect the various components shown in Fig. 1;

Figs. 2G-2H are schematic two-dimensional views showing optical fibers which
may be used to interconnect the various components of the photonic crystal
15 interferometric fiber optical gyroscope shown in Fig. 1;

Figs. 3A and 3B are schematic three-dimensional views of two exemplary
embodiments of the sensing coil shown in Fig. 1;

Fig. 4 is a schematic three-dimensional view of one embodiment of a photonic
crystal interferometric optical gyroscope system in accordance with this invention; and

20 Fig. 5 is a schematic block diagram of another embodiment of a photonic crystal
interferometric fiber optical gyroscope system employing a light source with increased
spectral width in accordance with this invention.

DISCLOSURE OF THE PREFERRED EMBODIMENT

Aside from the preferred embodiment or embodiments disclosed below, this invention is capable of other embodiments and of being practiced or being carried out in various ways. Thus, it is to be understood that the invention is not limited in its application to the details of construction and the arrangements of components set forth in the following description or illustrated in the drawings.

As discussed in the Background section above, conventional IFOGs suffer from several distinct drawbacks including, *inter alia*, a limited accuracy, limited sensitivity, limited ability to reduce ARW because of the diameter associated with conventional optical fibers, and limited spectral width light sources. Conventional IFOGs also have a relatively large package diameter (e.g., about three inches in diameter). The sensing coil of conventional IFOGs also utilizes optical fibers with significant bend loss, length loss, sensitivity to ionizing radiation, and thermal sensitivity.

Photonic crystal interferometric fiber optical gyroscope (IFOG) system 10, Fig. 1 of this invention typically includes light source 12 for providing primary beam of light 14 to beam controlling device 20 and photonic crystal sensing coil 16 (discussed below). Light source 12 may be an amplified spontaneous emission light source including a rare earth-doped fiber, a gas filled fiber, a liquid filled fiber, or a semiconductor material. The gas may include argon, helium, neon, carbon monoxide or carbon dioxide, and similar gases known to those skilled in the art. The liquid may be an organic dopant, such as rhodamine, or similar organic dopants known to those skilled in the art.

In other designs, light source 12 may be a stimulated emission light source, such as a laser, a gas filled fiber with a cavity, or a semiconductor material with a cavity (e.g.,

an LED), or a super-luminescent semiconductor material with a cavity (e.g., an SLD).

The gas may include argon, helium, neon, carbon monoxide or carbon dioxide, and similar gases known to those skilled in the art. In still other examples, light source 12 may be a thermally excited light source, such as an incandescent lsorce (e.g., a tungsten-halogen light source), a fluorescent light source (e.g., a fluorescent light bulb), an electro-luminescent light source, a chemical luminescent light source, a phosphorescence light source, or other broad-band light sources. In a preferred embodiment, light source 12 emits primary beam of light 14 having a wavelength of between 10 nm to 15,000 nm.

Beam controlling device 20 is configured to split primary beam 14 into counter-propagating beams 22 and 24 which travel in opposite directions in sensing coil 16. In one example, counter-propagating beam 22 travels in a clockwise direction about photonic crystal sensing coil 16, as indicated by arrow 26, and counter-propagating beam 24 travels in a counter-clockwise direction about photonic crystal sensing coil 16, as indicated by arrow 28, although this is not a necessary limitation of this invention, as the direction of the counter-propagating beams 22 and 24 may be reversed. Beam controlling device 20 is configured to direct the return of counter-propagating beams 22 and 24, indicated by arrows 30 and 32, respectively, to light detector 60 via coil splitter 42 and source splitter 40 (discussed in further detail below). The power caused by the interference of counter propagating beams 22 and 24 is measured by light detector 60 (also discussed in further detail below) and represents the phase shift between counter-propagating beams 22 and 24 which is indicative of the rate of rotation of photonic crystal sensing coil 16 about rotational axis 18, as indicated, by way of example only, by arrow 34.

Beam controlling device 20 includes source splitter 40 configured to direct light 14 from light source 12 into coil splitter 42. Source splitter 40 may be a fused-fiber coupler available from JDS Uniphase Corporation, San Jose, CA. Source splitter 40 is also configured to direct returning counter-propagating beams 22 and 24 from photonic crystal sensing coil 16 to light detector 60, as indicated by arrow 33. In one preferred design, source splitter 40 is a wide-band directional coupler, available from AOC Technologies, Inc., Pleasanton, CA, capable of processing light 14 (and returning counter-propagating beams 22 and 24) with increased spectral width in the range of about 10 to 1500 nm. Source splitter 40 may be a reciprocal splitter or a non-reciprocal splitter.

10 Beam controlling device also includes coil splitter 42 configured to divide light 14 emitted from light source 12, through source splitter 40, into two equal beams, e.g., counter-propagating beam 22 and counter-propagating beam 24. In one design, coil splitter 42 is a power splitter which is insensitive to the wavelength of light 14 (achromatic) and can process light 14 with increased spectral widths (e.g., in the range of about 10 nm to 15,000 nm). Coil splitter 42 can be custom designed with photonic crystal fiber (discussed below) or is commercially available from Gould Fiber Optics, Millersville, MD. Typically, coil splitter 42 is a reciprocal splitter.

15 Beam controlling device 20 also includes at least one modulator, such as modulator 44, and/or modulator 45, available from JDS Uniphase Corporation, San Jose, CA, which is configured to add a time-dependent phase shift to first counter-propagating beam 22 and/or second counter-propagating beam 24 to produce a non-reciprocating phase shift between counter-propagating beam 22 and counter-propagating beam 24. The non-reciprocating phase shift between counter-propagating beam 22 and counter-

propagating beam 24 constructively interfere (e.g., shift the power displacement) to modify the power and improve the sensitivity of photonic crystal IFOG system 10. In one design, modulator 44 and coil splitter 42 are integrated on an integrated optical chip (IOC), available from JDS Uniphase Corporation, San Jose, CA.

5 Light detector 60 detects light 35 (e.g., counter propagating beams 22 and 24) from source splitter 40. Light detector 60 is configured to convert the power of interfering counter-propagating beams 22 and 24, respectively, to an electrical signal. Light-detector 60 may be a PIN photo-detector, available from EG&G Optoelectronics, Salem, MA, an avalanche photo-detector, also available from EG&G Optoelectronics, a 10 photo-multiplier tube, available from Hamamatsu, Bridgewater, NJ, a bolometer, available from Infrared Laboratories, Tucson, AZ, a photo-resistive detector (also known as a photo-conductive detector), available from Hamamatsu, Bridgewater, NJ. When an electrical voltage is applied across light detector 60, the amount of electrical current drawn by light detector 60 is proportional to the amount of power on the surface of light 15 detector 60.

Photonic crystal sensing coil 16 is typically formed by winding a photonic crystal fiber which has a gas-solid structure that confines light by total internal reflection, or with a band gap fiber which confines light by employing an optical band gap (both discussed in detail below). The gas of the gas-solid structure of the photonic crystal fiber may be 20 air, an inert gas, or an active gas. In a preferred embodiment, the photonic crystal fiber and band gap fiber have an outer diameter of about 70 nm. Utilizing photonic crystal fibers or band gap fibers with decreased diameter to manufacture photonic crystal sensing coil 16 reduces the ARW (e.g., improves accuracy of IFOG system 10) because ARW is

proportional to the square of the fiber diameter. Reducing the diameter of the optical fibers also decreases the packing size of IFOG system 10. Moreover, photonic crystal fibers and band gap fibers, as employed in accordance with this invention, also decrease bend loss and length loss of photonic crystal sensing coil 16. These fibers also are less sensitive to gamma radiation, are less thermally sensitive, and eliminate the need to use dopants to confine light in photonic crystal sensing coil 16.

5 Photonic crystal sensing coil 16 may be made with photonic crystal fiber 70,

Fig. 2A which includes solid region 72 surrounded by solid clad 74 having a plurality of hollow channels 76 (which contain a gas, such as air, an inert gas, or an active gas)

10 configured to provide an index of refraction difference between core region 72 and clad 74 that confines light in core 72 by totally reflecting the light on clad 72. In a

preferred design, photonic crystal fiber 70 is configured to propagate a single mode of light. Photonic crystal fiber 70 may include jacket 78 surrounding clad 72. In one

example, the outer diameter of photonic crystal fiber 70, indicated by arrow 79, is in the range of about 20 to 250 μm . In other preferred embodiments, the outer diameter of photonic crystal fiber 70 is about 70 μm . In other designs, the outer diameter of photonic crystal fiber 40 is about 40 μm . Solid core 72 and solid clad 74 are typically made of silica, plastic, or similar dielectric materials known to those skilled in the art.

15 Photonic crystal sensing coil 16, Fig. 1 may also be formed with band gap

fiber 80, Fig. 2B which includes hollow core region 82 surrounded by solid clad 84.

Solid clad 84 includes a plurality of hollow channels 86 which create a band gap effect which confines the majority of light in hollow core region 82. Band gap fiber 80 is also typically configured to propagate a single mode of light. Band gap fiber 80 may also

include jacket 88. Band gap fiber 80 has similar dimensions to photonic crystal fiber 70, *supra*. Clad 84 of band gap fiber 80 is ideally made of silica, plastic, or similar dielectric materials known to those skilled in the art.

Band gap fiber 90, Fig. 2C may also be used to form photonic crystal sensing
5 coil 16, Fig. 1. Band gap fiber 90 includes hollow core region 92 surrounded by a solid
clad 94 which includes a plurality of alternating layers of solid dielectric material, such as
alternating layers 96, 98, 100, and 102, which are configured to create a band gap effect
that confines the majority of light in hollow core region 92. Band gap fiber 90 is also
configured to propagate a single mode of light. In one example, plurality of alternating
10 layers 96-102 are made of layers of dielectric material whose index of refraction
alternates between a high value and a low value. Solid clad 94 includes alternating layers
96-102 and functions similar to that of the cladding of the photonic and band gap crystal
fibers described above. Alternating layers 96-102 may be made from chalcogenide
glasses and thermoplastic polymer. Chalcogenide glasses are based on the chalcogen
elements sulfur, selenium and tellurium, and the addition of other elements, such as
15 germanium, arsenic, and antimony, lead to the formation of stable glasses. An example
of a suitable thermoplastic polymer includes a high glass-transition temperature
thermoplastic polymer, such as poly-ether-sulphone (PES). Band gap fiber 90 typically
includes jacket 104 surrounding clad 94. Band gap fiber 90 also has similar dimensions
20 as band gap fiber 80, Fig. 2B.

Photonic crystal sensing coil 16, Fig. 1 may also be formed by winding a photonic
crystal fiber 110, Fig. 2D which maintains polarization of light as it propagates and
propagates only one state of light. This design propagates only one state of light and is

one way to insure the light has traveled exactly the same path in each direction around photonic crystal sensing coil 16, Fig. 3. Photonic crystal fiber 110 includes asymmetric solid core region 112 surrounded by solid clad 114. Solid clad 114 includes plurality of asymmetrically spaced hollow channels 116 about asymmetric solid core region 112.

5 Plurality of hollow channels 116 produce an effective index of refraction difference between solid core region 112 and solid clad 114 to confine light by totally reflecting the light on plurality of hollow channels 116 of clad 114. The asymmetric spacing of hollow channels 116 and asymmetric core 112 also maintains the polarization of light and propagates only one state of light. Solid core 112 and clad 116 are typically made of

10 silica, plastic, or similar dielectric materials known to those skilled in the art. Photonic crystal fiber 110 typically includes jacket 117, surrounding clad 114 and has similar dimensions to the photonic crystal fibers and band gap of the photonic crystal sensing coil 16 discussed above.

Band gap fibers which maintain the polarization of light and propagate only one state light may also be used to form photonic crystal sensing coil 16. For example, band gap fiber 120, Fig. 2E includes asymmetrical hollow region for core 122 surrounded by solid clad 126 which includes plurality of asymmetrically spaced hollow channels 128 that create a band gap effect that confines a majority of light in hollow core 122 while maintaining the polarization of light and propagating only one state of polarization. Solid 20 clad 126 is ideally made of silica, plastic, or similar dielectrics. Band gap fiber 120 may also include jacket 130 and has similar dimensions to band gap fibers or photonic crystal fibers described above.

Photonic crystal sensing coil 16, Fig. 1 may also be formed with band gap

fiber 130, Fig. 2F which is configured to maintain the polarization of light and maintain only one state of polarization light. Fiber 130 includes asymmetric hollow core region 132 surrounded by solid clad 133 having a plurality of alternating asymmetric layers of solid dielectric material, such as asymmetric layers 134, 136, 138, 140, and 142 to 5 produce a band gap effect which confines a majority of light and hollow core 132 while maintaining the polarization of light and propagates only one state of light. Layers 134-142 are made of layers of dielectric material whose index of refraction alternates between a high value and a low value. The alternating layers of solid structure clad 133 may be made of chalcogenide glasses and thermoplastic polymer. Chalcogenide glasses are 10 based on the chalcogen elements sulfur, selenium and tellurium and the addition of other elements, such as germanium, arsenic, and antimony leads to the formation of stable glasses. A suitable thermoplastic polymer might be the high glass-transition temperature thermoplastic polymer, poly-ether-sulphone (PES). Band gap fiber 130 may also include jacket 143 and has similar dimensions to the band gap fibers discussed above.

15 Photonic crystal sensing coil 16, Fig. 1 is typically formed by winding the photonic crystal fibers or the band gap fiber, as delineated above and shown in Figs. 2A-2F, onto a mandrel or into a free standing coil. In one embodiment of this invention, photonic crystal sensing coil 16 includes 15,000 turns of photonic crystal fiber 70 or 110, Figs. 2A and 2D, respectively, or band gap fiber 80, 90, 120, 130, Figs. 2B, 2C, 2E, and 20 2F, respectively. As discussed above, using the photonic crystal fibers or band gap fibers with reduced outer diameter (e.g., 40 or 70 μm) to form photonic crystal sensing coil 16, Fig. 1 reduces the package size of photonic crystal IFOG system 10. For example, photonic crystal sensing coil 16, Fig. 3A has an outer diameter of approximately 0.75

inches, as indicated at 204, an inner diameter of about 0.5 inches, as indicated at 200, a height of approximately 0.75 inches, as indicated at 202, which results in a total package size of photonic crystal IFOG system 10 of about one cubic inch. To achieve the same precision or ARW a conventional IFOG made with non-photonic crystal fiber would have

5 to be significantly larger, and would have a volume of approximately ten cubic inches.

Photonic crystal sensing coil 16, Fig. 3B may be a medium sized coil which includes about 35,000 turns of the photonic crystal or band gap fibers delineated above. In this example, photonic crystal sensing coil 16 has an inner diameter of approximately 1.5 inches, as indicated at 210, a height of about 1 inch, as indicated at 212, and an outer 10 diameter of about 2.0 inches as indicated at 214, resulting in a package size of system 10 of about ten cubic inches. With this size coil and package size, photonic crystal IFOG system 10 can measure the angular rate with twenty times the precision of a comparable size conventional non-photonic crystal IFOG because the ARW for the photonic crystal IFOG system 10 would be twenty time smaller than a conventional IFOG of similar 15 dimension.

The result of using advance photonic crystal fibers and band gap fibers as discussed above and shown in Figs. 2A-2F to manufacture photonic crystal sensing coil 16, Fig. 1 of photonic crystal IFOG 10 of this invention significantly reduces the package size of system 10. The advanced photonic crystal or band gap fibers with 20 reduced diameter in photonic crystal sensing coil 16 also reduces ARW (e.g., improves accuracy) because ARW is proportioned to the square of fiber diameter. The photonic crystal fibers and band gap fibers also reduce bend loss, reduce length loss, are radiation insensitive, are thermal insensitive, and eliminate the need to dope the optical fibers.

Photonic crystal interferometric fiber optical gyroscope system 10 may also include optical wave guide 300, Fig. 1 configured to interconnect light source 12 and beam controlling device 20 and/or interconnect beam controlling device 20 and photonic crystal sensing coil 16. Although wave guide 300 as shown in Fig. 1 to interconnects 5 light source with beam controlling device 20 and beam controlling device 20 to photonic crystal sensing coil 16, this is not a necessary limitation of this invention, as light source 12 may be directly coupled to beam controlling device 20 and beam controlling device 20 may be directly coupled to photonic crystal sensing coil 16. Optical wave guide 300 may be a solid structure that confines light by total internal reflection (e.g., a conventional 10 optical fiber), a photonic crystal wave guide having a gas-solid structure that confines light by total internal reflection (e.g., a photonic crystal fiber described above), as discussed above, or a band gap wave guide that confines light by employing optical band gap (e.g., a band gap fiber as described above).

In one design, optical wave guide 300 may be configured as a conventional optical 15 fiber, such as optical fiber 310, Fig. 2G, which includes solid core 312 surrounded by solid clad 314 that confines light in solid core 312 by totally reflecting all light in solid core 312 on solid clad 314. In other examples, optical wave guide 300 may be optical fiber which is configured to maintain the polarization of light and to propagate one state of polarization, such as conventional optical fiber 350, Fig. 2H which includes solid 20 cylindrical core 352 surrounded by asymmetrically spaced solid rods 354 and 356 within clad 358. Fiber 350 is designed such that the index of refraction difference between core 352 and clad 358 confines light by total internal reflection while maintaining the polarization of light and propagating only one state of polarization of light.

One example of photonic crystal interferometric optical gyroscope system 10 of this invention is shown in Fig. 4 and depicts light source 12, source splitter 40, coil splitter 42, modulator 44, light detector 60, and photonic crystal sensing coil 16.

In one preferred embodiment of this invention, light source 12', Fig. 5, where like parts have been given like numbers, may be configured as a broad-band light source, such as a tungsten-halogen light source available from Ocean Optics, Dunedin, FL, to provide light 14 with an increased spectral width, such as light with a spectral width up to about 1500 nm, e.g., between about 100 to 1500 nm. In a preferred embodiment, light source 12' emits light 14 with a spectral width of about 1200 nm. As discussed in the 10 Background section, increasing spectral width of light 14 (and corresponding counter propagating beams 22 and 24) decreases the ARW because ARW is inversely proportional to the square root of the spectral width of the light in photonic crystal sensing coil 16. Because light source 12' emits light 14 with increased spectral width to photonic crystal sensing coil 16, the ARW is significantly reduced. In one example, such as sensing coil 16, Fig. 3A, the ARW is reduced to 0.001 degrees per square root hours (degree/ \sqrt{hr}). In other examples, such as sensing coil 16, Fig. 3B, the ARW is as low as 0.00005 degree/ \sqrt{hr} , which is about twenty times lower than a conventional IFOG utilizing conventional narrow band optical fibers. When compared to a conventional prior high performance gyroscope, e.g., an inertial grade gyroscope which has as a 15 maximum spectral width of about 30 nm, IFOG system 10' of this invention with light source 12' emitting light 14, in one example, with a spectral width of about 1200 nm results in a significant reduction of ARW. In this example, the ARW is reduced by a factor of about 6.3 (e.g., $1/\sqrt{30}$ nm versus $1/\sqrt{1200}$ nm).

Although specific features of the invention are shown in some drawings and not in others, this is for convenience only as each feature may be combined with any or all of the other features in accordance with the invention. The words "including", "comprising", "having", and "with" as used herein are to be interpreted broadly and comprehensively and are not limited to any physical interconnection. Moreover, any embodiments disclosed in the subject application are not to be taken as the only possible embodiments.

Other embodiments will occur to those skilled in the art and are within the following claims:

What is claimed is: